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DEPARTMENT OF LANDS, FORESTS, AND WATER RESOURCES

WATER RESOURCES SERVICE

KELOWNA CREEK WATER SUPPLY

FOR

GLENMORE AND ELLISON IRRIGATION DISTRICTS

DATE Apr. 1973

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0256957

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Hydraulic Engineer

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KELOWNA CREEK WATER SUPPLY
FOR
GLENMORE AND ELLISON IRRIGATION DISTRICTS

April, 1973

File: 0242512-52
0256957

D. E. Reksten, P.Eng.

Hydraulic Engineer

SYNOPSIS

This study of Kelowna Creek hydrology for Glenmore and Ellison Irrigation Districts was done at the request of Mr. J. V. Eby, Chief, ARDA Division, Water Investigations Branch.

Water is stored in South Lake (500 acre-feet), Postill Lake (4000 acre-feet) and Bulman Lake (1000 acre-feet) and is shared on the basis of 75% to Glenmore I.D. and 25% to Ellison I.D. Glenmore I.D. also has an 800 acre-foot capacity balancing reservoir.

Glenmore I.D. wishes to increase its irrigated acreage by up to 1200 acres. Based on the estimates of mean and drought year (1929-31) runoff derived in this study, under present conditions of demand and storage capacity, the Irrigation Districts could be supplied with water until August of the third drought year (equivalent to 1929-31) after a mean runoff year.

If 400 acres of the possible 1200 were added to Glenmore I.D., the existing 5500 acre-feet of storage would be depleted during August of the second drought year (equivalent to 1929-30) after a mean runoff year.

Using the above information as a guide, further storage calculations can be made using the Hydrology Division computer program for various demands and number of consecutive drought years.

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KELOWNA CREEK WATER SUPPLY

FOR

GLENMORE AND ELLISON IRRIGATION DISTRICTS

1. INTRODUCTION

This study of Kelowna Creek hydrology was done at the request of Mr. J. V. Eby, Chief, ARDA Division, Water Investigations Branch.

Glenmore and Ellison Irrigation Districts have developed the Kelowna Creek watershed (Fig. 2) under an agreement in which they share the stored water and runoff at the Glenmore-Ellison intake on a 75% - 25% basis, the greater share going to Glenmore Irrigation District. Water is stored in South Lake (500 ac-ft.), Postill Lake (4000 ac-ft.) and Bulman Lake (1000 ac-ft.). Glenmore Irrigation District also has a balancing reservoir (McKinley reservoir) of 800 ac-ft.

Glenmore Irrigation District wishes to increase its irrigated acreage by up to 1200 acres. There is also a proposal to have Ellison I.D. supply the Scotty Creek I.D. with about 200 ac-ft. of water during a dry year such as 1970 when Scotty Creek I.D. was short of water.

This study estimates runoff in each of the reservoir sub-basins and unregulated runoff at the joint intake in mean and drought runoff years. Storage calculations are made for conditions similar to the 1929-31 drought recorded in the Okanagan basin. (A description of the procedure used to compute monthly storage conditions is given in the Appendix).

The results of the storage calculations indicate that with the present demand and storage capacity, storage would be depleted in August of the third drought year (1931). 1016 ac-ft. would be left at the end of the second drought year and 1737 ac-ft. left at the end of the first drought year.

If 400 acres of irrigable land were added to the system (additional demand of 800 ac-ft.) 346 ac-ft. of storage would be in place at the end of the first drought year and storage would be depleted by August of the second drought year (1930).

Glenmore I.D. holds a licence to store 560 ac-ft. in the Conroy Creek basin tributary to Kelowna Creek. At the most suitable damsite the mean annual runoff is estimated at 210 ac-ft. Developing storage in this basin would not appear to be worthwhile.

2. MEAN ANNUAL RUNOFF

2.1 RUNOFF FROM BASIN CHARACTERISTICS

Using multiple regression analysis, equations to estimate 1971 runoff using basin physiographic characteristics have been derived for the April-July period. Two equations used for this study are shown in Table 1 and 2. Not all the independent variables in these equations are significant at the 5% level. They are included in the equations as they reduced the percent estimating error for the Bulman Creek (BU) and Vernon Cr. (VE) sub-basins which are in the Kelowna Creek area. Both results for each sub-basin are averaged to yield 1971 April-July runoff. Based on the 1971 streamflow data used to derive these equations and median basin elevation the ratio of April-July to annual runoff was determined for 500 ft. elevation bands. For the 4 sub-basins in this study the ratio is 0.91 and yields the following estimates of 1971 annual runoff.

	<u>Median Basin Elevation</u> (ft.)	<u>1971 Annual Runoff</u> (in.)
Total basin	4620	10.06
South Lake	4830	12.46
Postill Lake	4860	12.53
Bulman Lake	4680	9.68

Based on an analysis of Okanagan Lake natural tributary inflow data (Reference 1) and 1967-71 natural streamflow data for 7 sub-basins, it is estimated that 1971 annual runoff in the Kelowna Creek basin is 25% above the long-term mean (1921-71). Reducing the above runoff estimates by 25% gives the following mean annual runoff estimates.

	<u>Mean Annual Runoff</u> (in.)
Total basin	8.04
South Lake	9.96
Postill Lake	10.03
Bulman Lake	7.74

2.2 UBC AVERAGE RUNOFF ESTIMATES

UBC's runoff-elevation relationship described in "Average Flows in the Tributary Basins" (Reference 2) gives the estimated mean annual runoff in 500-ft. elevation bands in the Kelowna Creek basin. The results using the UBC estimates are:

	<u>Mean Annual Runoff</u> (in.)
Total basin	6.66
South Lake	9.08
Postill Lake	9.07
Bulman Lake	7.53

2.3 GRID SQUARE METHOD

Mean annual runoff estimates for grid squares covering the Kelowna Creek basin (Reference 3) were weighted by area within the sub-basins to yield the following estimates. Mean basin elevation was calculated in the same way, based on the mean grid square elevations.

	<u>Elevation</u>	<u>Mean Annual Runoff</u> (in.)
Total basin	4320	8.1
South Lake	4890	11.0
Postill Lake	4820	10.9
Bulman Lake	4640	10.0

2.4 VERNON CREEK BASIN RUNOFF ESTIMATES

C. H. Coulson (Reference 4) has derived a runoff-elevation relationship for mean annual runoff using natural streamflow data for the 1969-71 period. The relationship is in the form of a curve described by squared and cubed values of elevation. On the basis of 500-ft. elevation bands mean annual runoff is estimated as:

	<u>Mean Annual Runoff</u> (in.)
Total basin	6.4
South Lake	9.4
Postill Lake	9.5
Bulman Lake	6.7

2.5 SUMMARY

The results of the four estimating methods are shown in Table 3. For the total basin above the intake, the estimate used in this study is the average of the 4 methods, or 7.3 in. For the South Lake, Postill Lake

and Bulman Lake sub-basins, the results of 3 methods are averaged. The grid square estimate is not used as these sub-basins are much smaller than the area of the 5 km. grid squares for which data were compiled in the grid square report. The mean annual runoff for South Lake, Postill Lake and Bulman Lake sub-basins is 9.5 in., 9.5 in., and 7.3 in. respectively.

3. MINIMUM ANNUAL RUNOFF

Three estimating techniques are used to estimate minimum or drought condition runoff similar to the amounts which occurred in the Okanagan basin during the period 1929-31. The UBC estimates and Coulson's estimates for Vernon Creek basin are based on 1970 streamflow data; 1970 runoff was as low as that during the 1929-31 drought period. The third estimate is based on the ratio of 1929-31 runoff to mean runoff as determined in a previous study of Mission Creek hydrology.

3.1 UBC MINIMUM RUNOFF ESTIMATES

In the report "Flows in the Main Tributary Basins," (Reference 5) estimates of 1970 runoff for each 500 ft. elevation band are given. 1929-31 runoff is then given as 98%, 93% and 79% of 1970 runoff. Data in this report results in the following annual runoff estimates:

	<u>Annual Runoff (in.)</u>			
	<u>Total Basin</u>	<u>South Lake</u>	<u>Postill Lake</u>	<u>Bulman Lake</u>
1970	4.2	5.9	5.9	4.4
1929	4.1	5.8	5.8	4.3
1930	3.9	5.5	5.5	4.1
1931	3.3	4.7	4.7	3.5

3.2 VERNON CREEK BASIN RUNOFF ESTIMATES

C. H. Coulson's study (Reference 4) estimates 1970 annual runoff for 500 ft. elevation bands for the Vernon Creek watershed. To obtain 1929-31 data for this report, Okanagan Lake natural tributary inflow data (1921-71) were analyzed to obtain the relationship between 1970 runoff and that during the 1929-31 drought. These data show that 1929-31 runoff is 102%, 95% and 88% of 1970 runoff, resulting in the following estimates:

	<u>Annual Runoff (in.)</u>			
	<u>Total Basin</u>	<u>South Lake</u>	<u>Postill Lake</u>	<u>Bulman Lake</u>
1970	3.8	6.0	6.2	3.5
1929	3.9	6.1	6.3	3.6
1930	3.6	5.7	5.9	3.3
1931	3.3	5.3	5.5	3.1

3.3 MISSION CREEK HYDROLOGY ESTIMATES

In the report "Mission Creek Water Supply for Black Mountain Irrigation District" it was estimated that 1929, 1930 and 1931 were 57%, 53%, and 50% of the long-term mean. Using the mean runoff for each sub-basin estimated in Sec. 2.5, and assuming that the drought years have the same departure from the mean as the Mission Creek basin, the following estimates can be made:

	<u>Annual Runoff (in.)</u>			
	<u>Total Basin</u>	<u>South Lake</u>	<u>Postill Lake</u>	<u>Bulman Lake</u>
Mean	7.3	9.5	9.5	7.3
1929	4.2	5.4	5.4	4.2
1930	3.9	5.0	5.0	3.9
1931	3.6	4.8	4.8	3.6

3.4 SUMMARY

Estimates of the 1929-31 annual runoff are tabulated in Table 4. The average of the three estimating techniques is the estimate for each sub-basin used in this study. These values are shown in Table 4.

4. MONTHLY RUNOFF DISTRIBUTION

The monthly distribution of runoff is based on streamflow data collected in 1970 and 1971 in the Okanagan basin. The gauged sub-basins were assigned to 500 ft. elevation bands on the basis of median basin elevation. The monthly distribution is expressed as per cent of annual, and the average of the percentages for the sub-basins in each elevation band for each month computed.

The monthly distribution for 1970, a very low runoff year, is assumed to be valid for the 1929-31 drought years. The 1971 monthly distribution is used for mean runoff years as 1971, although an above average runoff year, is the only year fairly close to average with enough data available to establish the variation of monthly runoff distribution with elevation.

The 4 sub-basins in this study are in the 4500 to 5000 ft. median elevation range. The runoff distribution for these basins is as follows:

Monthly Runoff Distribution
(% of annual)

	<u>Oct-Mar.</u>	<u>Apr.</u>	<u>May.</u>	<u>June.</u>	<u>July.</u>	<u>Aug.</u>	<u>Sept.</u>
Mean Runoff Year .	12.0	4.0	49.5	26.0	4.5	2.0	2.0
Minimum Runoff Year	14.0	4.0	52.0	22.0	4.0	2.0	2.0

5. RESERVOIR EVAPORATION

To determine net inflow to the storage reservoirs for making storage calculations it is necessary to estimate lake evaporation losses.

The Atmospheric Environment Service, Can. Dept. of the Environment has estimated mean monthly lake evaporation on a grid square basis for the Okanagan basin. The estimates for each of the Glenmore-Ellison reservoirs are listed below in inches:

	<u>South Lake</u>	<u>Postill Lake</u>	<u>Bulman Lake</u>
Oct.-Mar.	0.9	0.9	1.0
April	1.6	1.6	1.7
May	3.3	3.3	3.4
June	3.8	3.8	3.9
July	4.9	4.9	5.0
August	4.3	4.3	4.4
September	<u>2.4</u>	<u>2.4</u>	<u>2.5</u>
Annual	21.2	21.2	21.9

In the Coulson report (Reference 4) mean annual and maximum annual lake evaporation for upland lakes (approximately 4400 ft. elev.) is given as 15.67 in. and 17.85 in. respectively. The figures tabulated above appear to be high on the conservative side and will be used for a mean and minimum runoff year.

To determine the amount of evaporation loss, the reservoir surface area at the spillway elevation is used in the storage calculations in Sec. 7.

6. DEMAND

Demand data used in this study was supplied by the ARDA Division and is given below for Glenmore and Ellison Irrigation Districts. 3.7% of the Glenmore I.D. demand is for domestic use while an even smaller proportion is required for domestic use for Ellison I.D.

	<u>Demand (ac.-ft.)</u>	
	<u>Glenmore</u>	<u>Ellison</u>
Oct.-Mar.	42	0
April	12	0
May	996	332
June	1,055	363
July	1,152	395
August	1,057	363
September	374	127
	<u>4,648</u>	<u>1,580</u>

7. STORAGE CALCULATIONS

A computer program has been devised by the Hydrology Division to perform calculations on runoff and demand to yield month-end storage in place. Because Glenmore I.D. has an 800 ac-ft. balancing reservoir (McKinley reservoir) below the joint Glenmore-Ellison intake, the computer program was used to obtain the monthly runoff available at the diversion and the rest was calculated by hand.

The following description of the operation of the Glenmore-Ellison system was provided by the ARDA Division. "Fall runoff from Kelowna Creek below the storage is diverted through the flume and Glenmore Syphon (maximum capacity 1500 ac-ft/month) to the Balancing Reservoir, until this fills, or cold weather necessitates the draining of the flume and syphon. Glenmore domestic water is supplied through the winter months by drawing on the storage in this Balancing (McKinley) Reservoir. In the Spring the flume/syphon is opened again to top up the Balancing Reservoir, to supply "flood-water" to the dry-farmed acreage and then to supply irrigation water when the season begins. The upper storage reservoirs are opened when the freshet can no longer meet demand, usually around mid-June. At this point "flood-water" is arbitrarily cut-off. In 1971, storage was not used till July 1, and "flood-water" was supplied to 50 acres all season."

"When the dams are opened, South Lake, Bulman Lake and Postill Lake are normally drawn down equally. Just downstream from the intake on Kelowna Creek the flow to Glenmore and Ellison is separated and recorded over weirs. In Ellison Irrigation District, irrigation water is "ordered" to eliminate

fluctuations in demand as there is no balancing reservoir. Minor reductions in the demand cause the supply to overflow to the Glenmore system."

Two storage runs are made in this report. Storage calculations are made for a mean runoff year followed by three drought years (1929-31) first for the existing demand and secondly for a demand which assumes an additional 400 acres of irrigation. A detailed description of the calculating procedure is given in the Appendix. The results of the two storage runs are tabulated in Table 5 and 6 and can be summarized as follows.

Run 1

It is assumed that all reservoirs are empty at the beginning of the mean runoff year. By the end of June a total of 5161 ac-ft. are in place in upstream reservoirs and McKinley reservoir is full, the demand up to May 30 being supplied from unregulated runoff. Excess water is available during May and June totalling 967 ac-ft. at McKinley reservoir and 1296 ac-ft. at the joint intake where it flows into Kelowna Creek. The carry-over storage of 2439 is assumed to be distributed as 1952 ac-ft. in Postill Lake and 487 ac-ft. in Bulman Lake with South Lake being emptied due to its small capacity. It is assumed that 300 ac-ft. are retained in McKinley reservoir.

In the following drought years it is evident that little, if any, water would be available for "flood-water" irrigation. The 75% - 25% sharing of upstream storage can be met without difficulty during the drought period.

Under the assumed demand and operating conditions, the existing system would provide adequate water through two drought years and up to August of the third year. By the end of September, the system would be deficient by 743 ac-ft.

Run 2

For this run it is assumed that the demand is increased by 800 ac-ft. by the addition of 400 acres of irrigable land to the system. The total upstream storage reaches 5162 ac-ft. at the end of June and McKinley reservoir is full. During May and June excess water is available amounting to 1296 ac-ft. at the joint intake and 615 ac-ft. at McKinley reservoir. The carry-over storage of 1842 ac-ft. is distributed as 0 in South Lake, 1625 ac-ft. in Postill Lake and 217 ac-ft. in Bulman Lake. It is assumed that McKinley reservoir carries over 350 ac-ft.

In the following drought year Glenmore I.D. requires 4165 ac-ft. from upstream storage, more than its 75% share of 3471 ac-ft., although 300 ac-ft. are retained in McKinley reservoir. Ellison I.D. requires 788 ac-ft. which is less than its share of 1157 ac-ft. Only 346 ac-ft. are carried over to the next drought year (1930).

Due to the low carry-over storage, increased demand and transmission losses, storage is depleted during August of the second drought year. By September 30 the deficiency amounts to 1412 ac-ft.

These two runs indicate that some additional demand could be accommodated depending on the number of consecutive drought years one wishes to design for. If the design was based on one drought year, 400

acres of land could be added. It is obvious that the addition of 1200 acres of irrigable land could not be considered with the present amount of storage.

8. ADDITIONAL STORAGE

Glenmore I.D. holds a licence on Conroy Creek for 560 ac-ft. of storage. A damsite was proposed in 1962 at the point shown in Figure 2. The area of this basin is 0.66 sq. mi. with a median elevation of 4570 ft. In Figure 3, estimates of mean annual runoff for South, Postill, and Bulman Lake basins are plotted against their median elevations. Based on this simple relationship, the mean annual runoff for the Conroy Creek basin above the proposed damsite is estimated at 6.0 in. or 210 ac-ft. Although based on a different area (0.53 sq. mi.), 210 ac-ft. compares with 109 ac-ft. estimated in a report by Wannop and Hirtle Engineering Ltd. dated April 15, 1963. Their conclusion that "further consideration of the proposed Conroy Creek reservoir is not warranted at this time" would still appear to be valid. Considering evaporation losses, and transmission losses, the useable storage would be something less than 210 ac-ft.

9. CONCLUSIONS

The results of this study must be qualified by the following points:

1. Monthly evaporation losses for calculating reservoir net inflow are based on the reservoir area at the spillway elevation. This provides a conservative net inflow estimate on the low side.
2. The operation of the reservoirs, reflected in how the carry-over storage is distributed to each reservoir at the end of the year, could be varied as well as the operation of McKinley balancing reservoir.
3. The year of lowest runoff, 1931, has a return period of roughly 50 years. The return period for three consecutive drought years such as 1929-31 would be much greater.

The storage calculations indicate that:

- (a) if the system is designed for a 1 year drought, 400 - 500 acres of irrigable land could be added to Glenmore I.D.
- (b) if the system is designed for a 2 year drought, no additional acreage could be accommodated.
- (c) there is not enough runoff available at the proposed Conroy Creek damsite to make further consideration worthwhile.
- (d) ignoring transmission and distribution losses from Ellison I.D. to Scotty Creek I.D., it would be possible to supply 200 ac-ft. of water to Scotty Creek I.D. from Ellison I.D.'s share of the joint water supply for 1 drought year under present storage and demand conditions.

RECOMMENDATIONS

ARDA Division personnel should make any further storage runs they feel necessary to cover all alternatives of storage operation, demand, etc., through the Hydrology Division.

Monthly data should be obtained on South Lake, Postill Lake, Bulman Lake and McKinley reservoir to provide month-end lake levels. Facilities for measuring the outflow from these reservoirs should be established in order that the estimates made in this study can be verified.

FORECAST EQUATIONS OK SUB-BASIN 1971 RO FROM BASIN CRTCS (NORTH) STATION RUN P

TABLE 1

LY 27 SURO2 - + 0.2626 PPN1 (X 1) SB = 0.1791 T = 1.47 PAR R = 0.8602
 + 0.0653 AR45P (X 7) SB = 0.0156 T = 4.19 PAR R = 0.8288
 + 0.7089 BRISE (X 12) SB = 0.5667 T = 1.25 PAR R = 0.4045
 - 2.6732 STAND. ERROR = 1.0379 F(3, 8) = 10.50
 MULT R = 0.8930 R SQUARED = 0.7975

YEAR	FORECAST RUN-OFF	OBSERVED RUN-OFF	DIFF	PERCENT ERROR	12 YEARS
19ES	6.605	7.880	-1.275	-16.2	
19TE	6.552	7.070	-0.518	-7.3	
19LY	4.087	4.780	-0.693	-14.5	
19LB	3.709	4.040	-0.271	-6.7	
19WB	5.578	4.940	0.638	12.9	
19WM	5.262	4.420	0.842	19.1	
19PE	7.313	8.150	-0.837	-10.3	
19CL	3.088	7.580	-4.492	-59.7	
19CO	1.021	1.900	-0.879	-48.4	
19EW	5.897	4.510	1.387	30.8	
19VE	4.341	4.280	0.061	1.4	
19BU	4.267	3.150	1.117	35.4	

SURO2 = April-July runoff (ac.ft./sq.mi. x .01)
 PPN1 = Jan.-Mar. precipitation (in.) (AES OKAGN5 model)
 AR45P = Percent of sub-basin area above 4500 ft. (%)
 BRISE = Basin rise (ft. x .001)

TABLE 2
OK SUB-BASIN 1971 RO FROM BASIN CRTCS (NORTH) STATION RUN T

YEAR	FORECAST RUN-OFF	OBSERVED RUN-OFF	DIFF	PERCENT ERROR	12 YEARS
1953	6.812	7.880	-1.068	-13.6	
1954	5.652	7.070	-1.418	-20.1	
1955	4.239	4.780	-0.541	-11.3	
1956	3.689	4.040	-0.351	-8.7	
1957	5.320	4.940	0.380	7.7	
1958	4.813	4.420	0.393	8.9	
1959	7.563	8.150	-0.587	-7.2	
1960	3.925	2.580	1.345	52.1	
1961	0.844	1.980	-1.136	-57.4	
1962	5.813	4.510	1.303	28.9	
1963	4.744	4.280	0.464	10.8	
1964	4.365	3.150	1.215	38.6	

BELEV = Median basin elevation (ft. x .001)

$(X_{11}) = 0.1739$ $SB = 0.1739$ $T = 0.287$ $PAR R = 0.2797$
 $(X_{11}) = 0.9820$ $SB = 0.9820$ $T = 3.99$ $PAR R = 0.7961$
 $R SQUARED = 0.7486$ $F(2, 9) = 13.40$

TABLE 3 SUMMARY OF MEAN ANNUAL RUNOFF ESTIMATES

METHOD	BASIN RUNOFF (in.)			
	SOUTH	POSTILL	BULMAN	TOTAL
Basin Characteristics	10.0	10.0	7.7	8.0
U.B.C.	9.1	9.1	7.5	6.7
Grid Square	11.0	10.9	10.0	8.1
Vernon Creek	9.4	9.5	6.7	6.4
Average in.	9.5	* 9.5	* 7.3	* 7.3
Ac-ft.	1270	4200	1630	12,300

* Grid square estimate not included.

TABLE 4 SUMMARY OF MINIMUM ANNUAL RUNOFF ESTIMATES

METHOD	BASIN RUNOFF (in.)											
	SOUTH			POSTILL			BULMAN			TOTAL		
	1929	1930	1931	1929	1930	1931	1929	1930	1931	1929	1930	1931
U.B.C.	5.8	5.5	4.7	5.8	5.5	4.7	4.3	4.1	3.5	4.1	3.9	3.3
Vernon Cr.	6.1	5.7	5.3	6.3	5.9	5.5	3.6	3.3	3.1	3.9	3.6	3.3
Mission Cr.	5.4	5.0	4.8	5.4	5.0	4.8	4.2	3.9	3.6	4.2	3.9	3.6
Average (in.)	5.8	5.4	4.9	5.8	5.5	5.0	4.0	3.8	3.4	4.1	3.8	3.4
(ac-ft.)	773	719	653	2570	2430	2210	895	851	762	6900	6400	5720

ELLENHORE-ELLISON FUTURE STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE

RESERVOIR AREA STORAGE (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT) (ACRE-FT)

RESERVOIR	AREA (ACRE)	STORAGE (ACRE-FT)	DCT-MAR	APR	MAY	JUN	JUL	AUG	SEP
1	48.0	400.0	0.00	1.00	3.00	3.00	0.00	0.00	0.00
2	226.0	4000.0	0.00	1.00	3.00	3.00	0.00	0.00	0.00
3	80.0	1000.0	0.00	1.00	3.00	3.00	0.00	0.00	0.00

1 EDWIN LAKE RESERVOIR
2 POSTILL LAKE RESERVOIR
3 BURNING LAKE RESERVOIR

MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE

ANNUAL MAT RUNOFF ABOVE INTAKE = 12300 ACRE-FT
TRANSMISSION LOSS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

RESERVOIR (ACRE-FT)

1 1270 4.0 40.5 26.0 4.5 2.0 2.0
2 1200 4.0 40.5 20.0 4.5 2.0 2.0
3 1830 6.0 49.5 26.0 4.5 2.0 2.0

MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE MONTHLY STORAGE CAPACITY STORAGE

ANNUAL MAT RUNOFF ABOVE INTAKE = 12300 ACRE-FT
TRANSMISSION LOSS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

RESERVOIR (ACRE-FT)

1 1270 4.0 40.5 26.0 4.5 2.0 2.0
2 1200 4.0 40.5 20.0 4.5 2.0 2.0
3 1830 6.0 49.5 26.0 4.5 2.0 2.0

RESERVOIR (ACRE-FT)

1 1270 4.0 40.5 26.0 4.5 2.0 2.0
2 1200 4.0 40.5 20.0 4.5 2.0 2.0
3 1830 6.0 49.5 26.0 4.5 2.0 2.0

RESERVOIR (ACRE-FT)

1 1270 4.0 40.5 26.0 4.5 2.0 2.0
2 1200 4.0 40.5 20.0 4.5 2.0 2.0
3 1830 6.0 49.5 26.0 4.5 2.0 2.0

RESERVOIR (ACRE-FT)

1 1270 4.0 40.5 26.0 4.5 2.0 2.0
2 1200 4.0 40.5 20.0 4.5 2.0 2.0
3 1830 6.0 49.5 26.0 4.5 2.0 2.0

ELLENORE-ELECTRON TOY-THECUMBER CRT STORAGE RUN 12/23/67

NUMBER OF RESERVOIRS = 2

RESERVOIR	AREA (ACRES)	STORAGE CAPACITY (ACRE-FT)	OCT-MAR	APR	MAY	JUN	JUL	AUG	SEP
1	28.0	800.0	2.38	3.50	4.50	4.50	4.50	4.50	5.46
2	524.0	4000.0	4.00	3.00	4.00	4.00	4.00	4.00	4.46
3	80.0	1000.0	1.00	1.00	1.00	1.00	1.00	1.00	1.00

1 SOUTH LAKE RESERVOIR

2 POSTILL LAKE RESERVOIR

3 BULMAN LAKE RESERVOIR

YEARS NEAR YEAR

MONTH	ANNUAL NET EMPLOY ABOVE INTAKE = 12300 ACRE-FT	OCT	MAR	APR	MAY	JUN	JUL	AUG	SEP
TRANSMISSION LOSS	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
RESERVOIR	1270	12.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
	1200	12.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
	1200	12.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0

RESERVOIR (ACRE-FT)

MONTH	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES
OCT-MAR	1478	852	149	487	191	0	574	42	574	42	574	42	574
APR	442	208	64	138	97	0	318	0	318	0	318	0	318
MAY	638	384	257	815	707	302	2868	1224	2868	1224	2868	1224	2868
JUN	378	170	232	710	490	143	1768	1224	1768	1224	1768	1224	1768
JUL	240	142	104	38	11	0	350	0	350	0	350	0	350
AUG	240	142	104	38	11	0	350	0	350	0	350	0	350
SEP	240	142	104	38	11	0	350	0	350	0	350	0	350
ANNUAL	12216	7050	5100	1180	3001	1821	0.000	1206	8406	1936	5141	5448	1911

CARRY-OVER STORAGE

	0	1678	217											
--	---	------	-----	--	--	--	--	--	--	--	--	--	--	--

* max. capacity of syphon and flume to McKinley is 1500 ac.ft./month

YEAR 1970

MONTH	ANNUAL NET RUNOFF ABOVE INTAKE = 4900 ACRE-FT	OCT	MAR	APR	MAY	JUN	JUL	AUG	SEP
TRANSMISSION LOSS	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
RESERVOIR	2570	14.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
	2570	14.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
	2570	14.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0

RESERVOIR (ACRE-FT)

MONTH	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES
OCT-MAR	556	593	373	109	343	120	568	0	573	42	581	0	581	0	581	0	581	0	581	0
APR	328	210	134	225	177	67	124	0	124	0	124	0	124	0	124	0	124	0	124	0
MAY	478	272	286	793	677	204	2094	18	2094	18	2094	18	2094	18	2094	18	2094	18	2094	18
JUN	276	170	106	11	11	118	358	378	358	378	358	378	358	378	358	378	358	378	358	378
JUL	138	85	53	-1	-20	-3	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0
AUG	138	85	53	-1	-20	-3	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0
SEP	138	85	53	-1	-20	-3	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0
ANNUAL	3908	4238	2661	909	2178	788	2687	186	2886	1880	1937	5448	0	687	181	785	3471	694	4165	1933

CARRY-OVER STORAGE

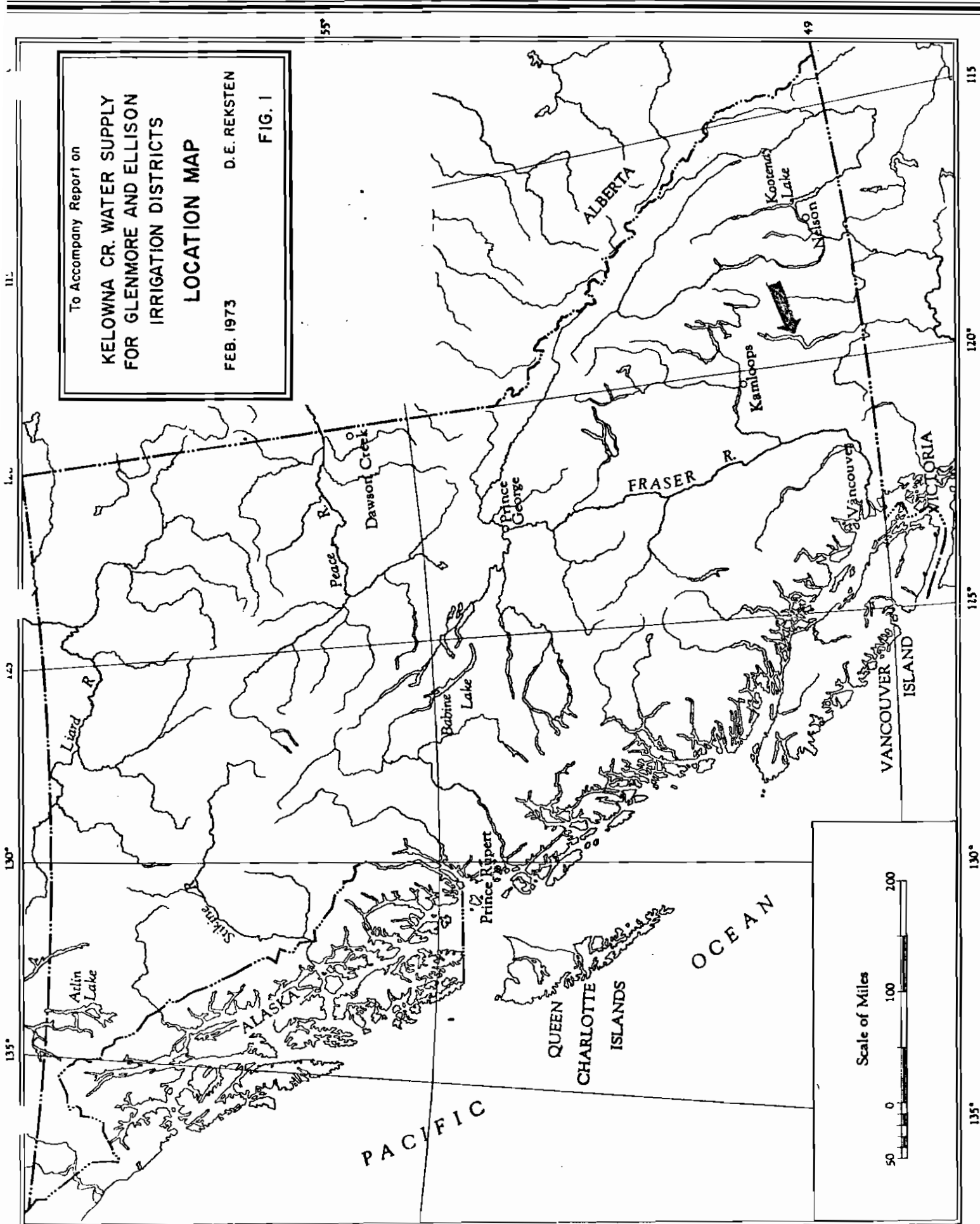
	0	160	86																	
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* max. capacity of syphon and flume to McKinley is 1500 ac.ft./month

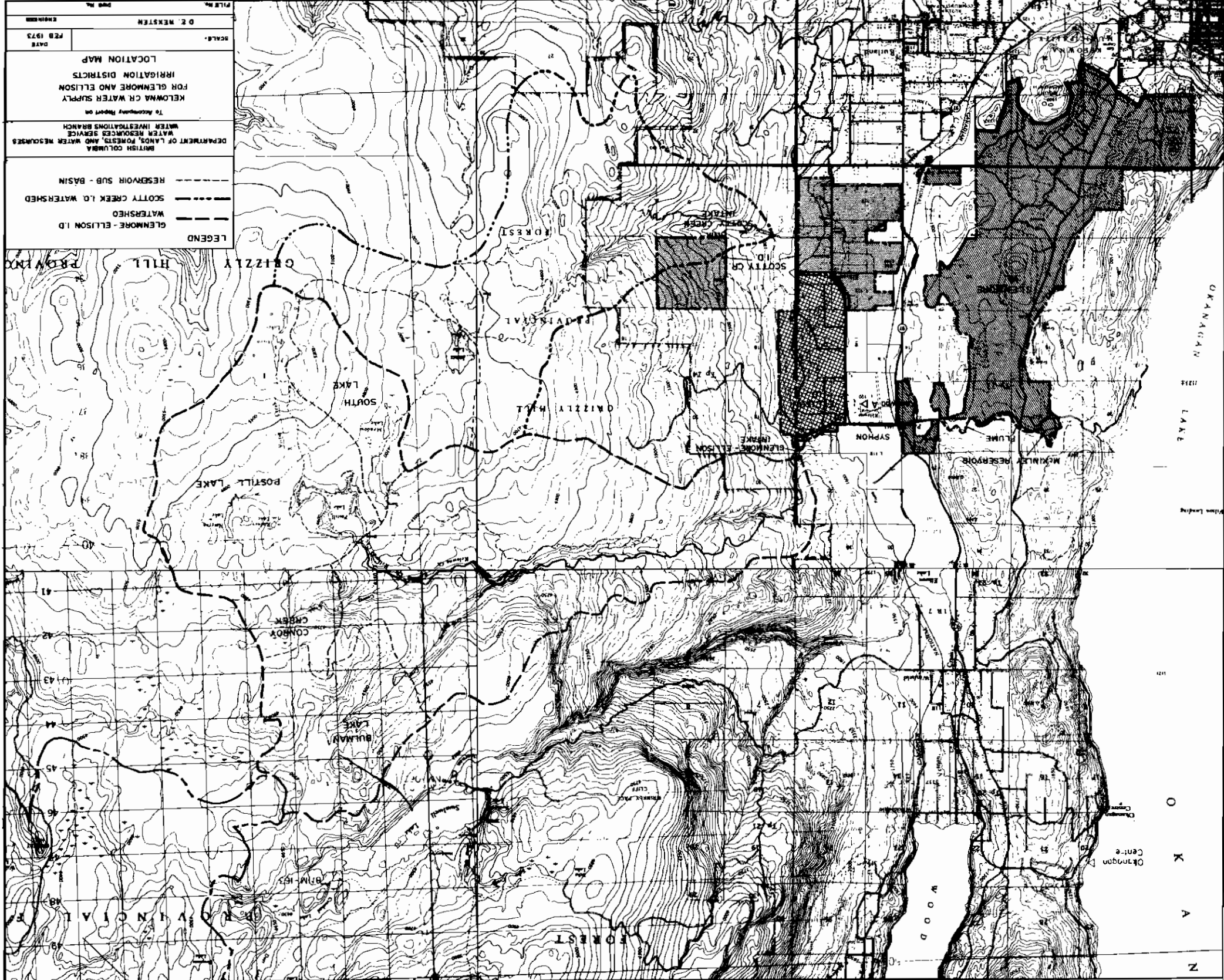
YEAR 1971

MONTH	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES
OCT-MAR	556	593	373	109	343	120	568	0	573	42	581	0	581	0	581	0	581	0	581	0
APR	328	210	134	225	177	67	124	0	124	0	124	0	124	0	124	0	124	0	124	0
MAY	478	272	286	793	677	204	2094	18	2094	18	2094	18	2094	18	2094	18	2094	18	2094	18
JUN	276	170	106	11	11	118	358	378	358	378	358	378	358	378	358	378	358	378	358	378
JUL	138	85	53	-1	-20	-3	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0
AUG	138	85	53	-1	-20	-3	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0
SEP	138	85	53	-1	-20	-3	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0	-34	0
ANNUAL	3908	4238	2661	909	2178	788	2687	186	2886	1880	1937	5448	0	687	181	785	3471	694	4165	1933

To Accompany Report on
**KELOWNA CR. WATER SUPPLY
 FOR GLENMORE AND ELLISON
 IRRIGATION DISTRICTS**
LOCATION MAP
 FEB. 1973 D. E. REKSTEN
 FIG. 1

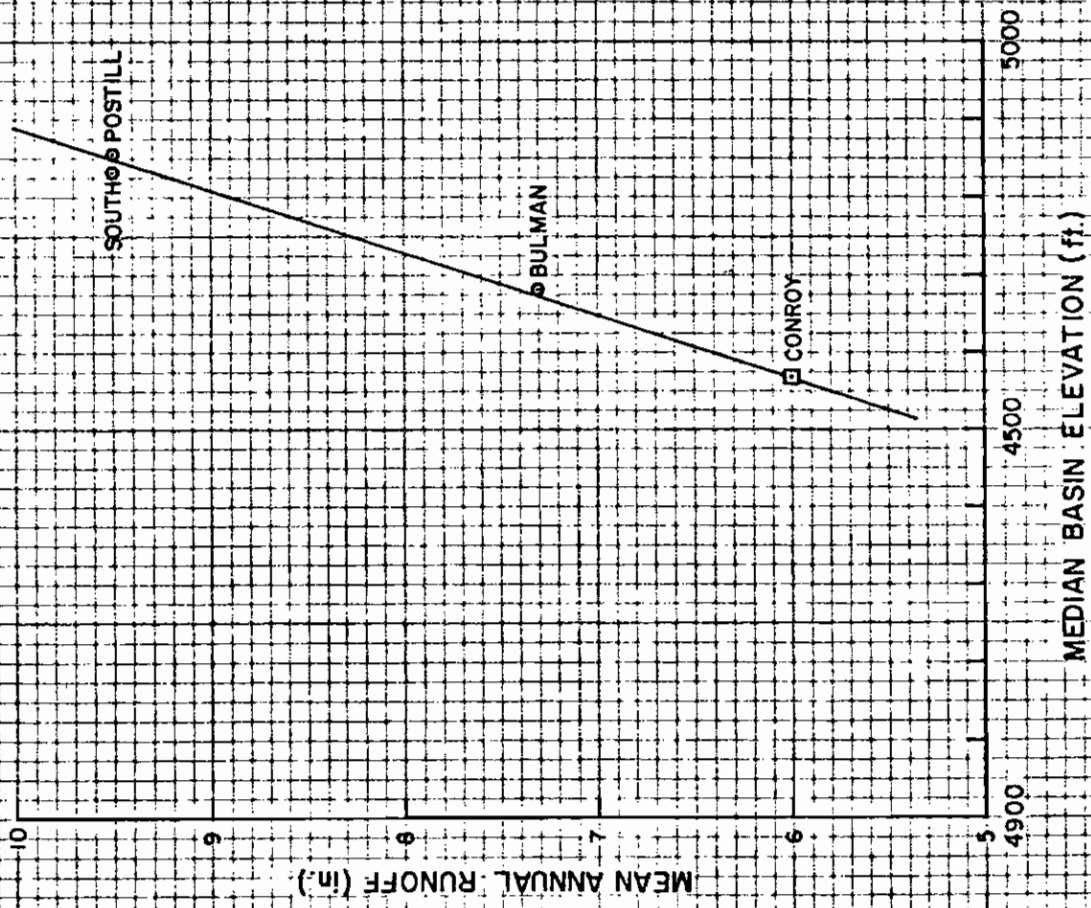


FILE NO. _____
 O.E. NEXSTEN
 ENGINEER
 SCALE: _____
 DATE: FEB 1973
LOCATION MAP
 FOR GLENMORE AND ELLISON
 IRRIGATION DISTRICTS
 KELOWNA CR WATER SUPPLY
 TO ACCOMPANY REPORT ON
 BRITISH COLUMBIA
 DEPARTMENT OF LANDS, FORESTS, AND WATER RESOURCES
 WATER INVESTIGATIONS BRANCH
LEGEND
 ----- GLENMORE - ELLISON I.D.
 ----- WATERSHED
 ----- SCOTTY CREEK I.D. WATERSHED
 ----- RESERVOIR SUB - BASIN



Okanagan
 Centre

OKANAGAN LAKE
 Okanagan
 Centre



BRITISH COLUMBIA
 DEPARTMENT OF LANDS, FORESTS, AND WATER RESOURCES
 WATER RESOURCES SERVICE
 WATER INVESTIGATIONS BRANCH

To Accompany Report on
**KELOWNA CR. WATER SUPPLY FOR
 GLENMORE AND ELLISON IRRIGATION DISTRICTS**
 D. E. REKSTEN

SCALE: VERT.
 HOR.
 SURVEY BY:

DATE
 FEB. 1973

FILE No. DWG. No. **FIG. 3**

ADDENDUM

Further storage calculations were done at the request of the ARDA Division using revised demands and storage capacities to obtain data on possible changes to the system.

Run A1 incorporates the following changes (figures in brackets are those used in Run 1):

(a) Storage Capacities

South	560 acre-feet	(500)
Postill	4,065 acre-feet	(4,000)

(b) Demand (acre-feet) (Estimated 1973)

	Glenmore	Ellison
October-March	85	10
April	24	3
May	1,063	335
June	1,181	369
July	1,293	402
August	1,185	369
September	<u>424</u>	<u>130</u>
	5,255 (4,648)	1,618 (1,580)

(c) Initial Conditions

For the initial conditions in Run 1 and 2, it was assumed that the reservoirs were empty at the beginning (October 1) of the mean runoff year. For Run 1A it was assumed that the reservoirs were half full at the beginning of the first drought year (1929). In Run 1, the total storage in place at the beginning of the first drought year was 2,439 acre-feet. In Run 1A, the total

storage in place is assumed to be 2,800 acre-feet, roughly half of the total storage capacity of 5,625 acre-feet.

Based on the above changes, the estimated 1973 demand could be satisfied until September of the second drought year (1930).

Run A2 was made to determine the additional storage required to satisfy the maximum projected demand. The storage capacities were increased arbitrarily by an amount estimated to satisfy the increased demand into the second drought year.

The following data were used (figures in brackets are those used in Run A1):

(a) Storage Capacities

South	1,060 acre-feet	(560)
Postill	5,565 acre-feet	(4,065)
Bulman	1,500 acre-feet	(1,000)

(b) Demand (acre-feet)

	Glenmore	Ellison
October-March	94	10
April	26	3
May	1,331	428
June	1,476	472
July	1,615	513
August	1,480	472
September	<u>528</u>	<u>165</u>
	6,550 (5,255)	2,063 (1,618)

(c) Initial Conditions

Same as Run 1A.

Under the above conditions a dependable water supply would be available until July of the second drought year. The feasibility of increasing the storage capacities of the three existing reservoirs was not considered. In any case, if one assumes that the optimum potential capacity of a reservoir is 80% of the mean annual inflow, Postill Lake and Bulman Lake would be over-developed with the assumed capacities and could not be used to their full potential. Based on present knowledge of the Kelowna Creek basin, it would appear that there is little possibility of increasing storage capacity to the degree necessary to satisfy the maximum projected demand during drought conditions.

Copies of the storage calculations are included in this addendum.

June 11, 1973

APPENDIX

STORAGE CALCULATIONS

The method of calculating month-end storage for Glenmore - Ellison reservoirs is best explained with reference to Fig. A1 and Table A1. The computer program for these calculations was derived by R. Wyman of the Hydrology Division. Because McKinley reservoir is downstream of the joint intake, some of the calculations were done by hand. The numbers below refer to the columns in Table A1.

The natural runoff, for the whole basin above the intake is estimated (1). From this is subtracted the total natural runoff into each reservoir sub-basin (2) to obtain the unregulated runoff (3). From the natural reservoir basin runoff, lake evaporation is subtracted to yield net inflow for each reservoir (4, 5 and 6). The net inflow stored each month for each reservoir is totalled (7) until the reservoirs reach their capacity and net inflow must be spilled (8). What is available each month at the intake (9) is the sum of spill (8) and unregulated runoff (3).

At this point it is assumed that Ellison I.D. demand (10) is taken off first. What is left is spilled to the balancing reservoir (11) up to the flume and syphon capacity of 1500 ac-ft. per month. The amount that cannot be handled is assumed to be lost to Kelowna Creek and included in spill to lake (14). From spill to McKinley, Glenmore I.D. demand (12) is taken and the rest goes to filling McKinley reservoir (13). When McKinley is full (800 ac-ft.), water is spilled to Okanagan Lake (14).

Appendix cont'd

The storage required for Ellison demand (15) is obtained by subtracting what is available at the intake (9) from the monthly demand (10). (If (9) is greater than (10), no storage is required.) A transmission loss of 20% of required storage during July - September (16) is added to the required storage (15) to obtain the storage used (17).

The storage required to satisfy the Glenmore I.D. demand (12) can be supplied either from upstream storage or the balancing (McKinley) reservoir. If Glenmore demand (12) is less than the spill to McKinley (11), no storage is required (18); in this case up to the end of June. In July, when storage is required, it is assumed that 450 ac-ft. are used from McKinley reservoir (13) and the balance is taken from upstream storage (18). The transmission loss (19) is added to this to obtain the storage used from upstream reservoirs (20). The storage used for Ellison I.D. (17) and Glenmore I.D. (20) are summed to yield the total upstream storage used (21). The storage in place (22) is the accumulated sum of the monthly total inflow stored (7) from which total storage used (21) is subtracted each month. This does not include the storage used from McKinley reservoir.

At the end of September in this example a total of 1842 ac-ft. is left in the 3 reservoirs. An assumed distribution of this carry-over storage to each reservoir must be made to begin calculations for the next year. This can be done on any basis as long as the 3 carry-over storages add up to 1842 ac-ft. In this example, reservoir 1 is assumed to be emptied because it has a high inflow in relation to its

Appendix cont'd

capacity (4). The other two are assumed to retain about 37% of their capacity in storage.

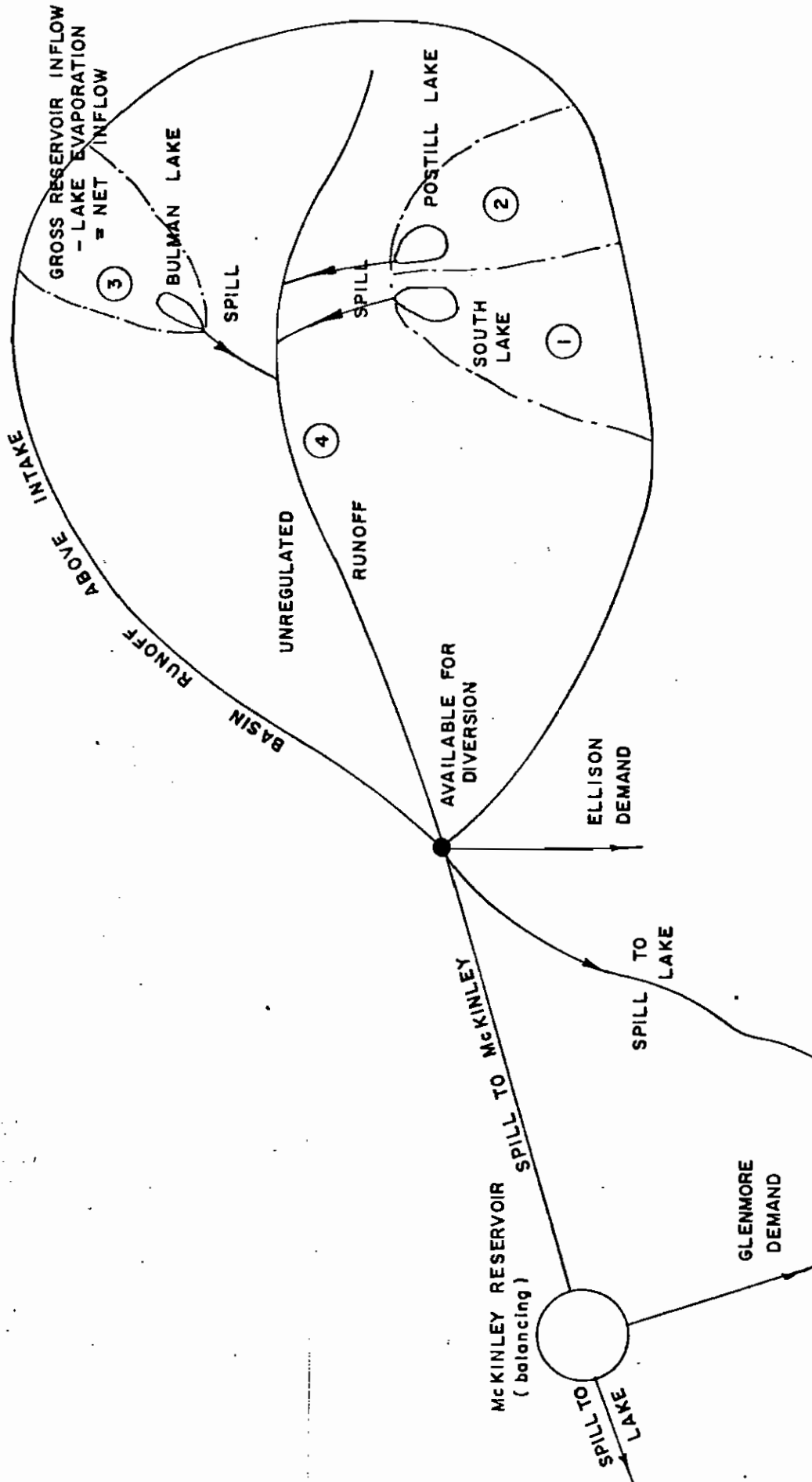
Calculations for the next year will take into account these carry-over storage amounts in each reservoir.

TABLE AI Storage Calculation Example

YEAR	RESERVE	ACRE-FT.	MONTH												AVE	SEC
			OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG			
12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300
			100	100	100	100	100	100	100	100	100	100	100	100	100	100
			0	0	0	0	0	0	0	0	0	0	0	0	0	0

MONTH	INFLW	OUTFLW	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	RES	ELLSOM		ELLSOM		TOTAL	
																STRS	USED	STRS	USED	STRS	
OCT	1478	532	1478	457	191	378	0	578	0	578	41	578	41	578	41	0	0	0	0	0	1014
NOV	6272	318	6272	2013	190	338	2074	348	2920	333	3858	112	3858	112	3858	112	0	0	0	0	4170
DEC	3158	3846	3158	1070	307	1727	1727	1727	1727	1727	1727	1727	1727	1727	1727	0	0	0	0	0	3463
JAN	513	319	513	28	97	329	329	329	329	329	329	329	329	329	329	0	0	0	0	0	1021
FEB	248	147	248	16	3	122	122	122	122	122	122	122	122	122	122	18	438	0	0	0	1775
MAR	201	147	201	0	0	32	32	32	32	32	32	32	32	32	32	0	0	0	0	0	2010
APR	1255	789	1255	3188	3981	1081	1081	1081	1081	1081	1081	1081	1081	1081	1081	1011	518	65	978	1969	3101
ANNUAL	12250	8000	12250	1180	1081	3200	1288	6406	1080	6141	6448	1011	518	65	978	1969	3101	2401	619	2401	5439

* Max. capacity of siphon and flume to McKinley is 1300 cfs./month.



SCALE: VERT. _____	DATE _____
HOR. _____	FILE No. _____
D. E. REKSTEN ENGINEER	
DWG. No. FIG A1	

TO ACCOMPANY REPORT ON
 KELOWNA CR. WATER SUPPLY FOR GLENMORE
 AND ELLISON IRRIGATION DISTRICTS
 WATERSHED MODEL FOR
 STORAGE CALCULATIONS

BRITISH COLUMBIA
 DEPARTMENT OF LANDS, FORESTS, AND WATER RESOURCES
 WATER RESOURCES SERVICE
 WATER INVESTIGATIONS BRANCH

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3. Obedkoff, W. : Application of the grid square method for estimating Okanagan sub-basin runoff, British Columbia Water Resources Service, December 1971.
4. Coulson, C. H. : Annual runoff relationship, Preliminary Report for Project 3, Kalamalka - Wood Lake Basin Water Resource Management Study, British Columbia Water Resources Service, December 1972.
5. Russell, S. O. : Flows in the main (Okanagan) tributary basins, Department of Civil Engineering, University of British Columbia, March 1972.